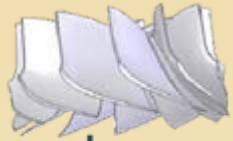




**Saint-Petersburg
State Polytechnic
University**

**Laboratory of
Applied
Mathematics and
Mechanics**



Multiprocessor simulations of turbulent diffusion flames

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Russia



Content

- **Motivation and work objectives**
- **Experiment and problem statement**
- **Simulation results**
 - **Test simulations**
 - **Comparative analysis of physical models**
 - **Calculating efficiency of clusters and models**
- **Conclusions**
- **Future work**

Introduction

- **Motivation**
 - **Computational Combustion is the most difficult area of Computational Fluid Dynamics (CFD)**
 - **Tight interaction between phenomena of different nature: turbulence, combustion and radiation**
 - **Wide spectrum of engineering applications: furnaces, turbines, engines, fires**
 - **Powerful computational software (Ansys Fluent etc.) and multiprocessor computers**

Introduction

- **Primary aim**

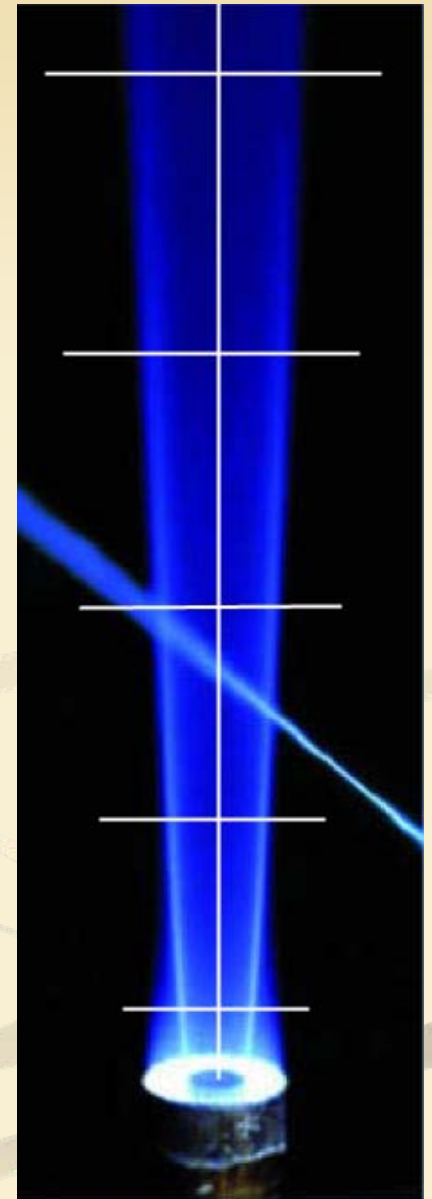
Accurate modeling of real-life problems like fires and industrial combustors using reliable verified models

- **Objectives**

- Pose model problem (test flame) with detailed statement and experimental data
- Examine conventional engineering models
- Research capabilities of advances chemistry models like slow chemistry and pollutant emissions
- Research capabilities of large eddy simulation turbulence model

Problem description

- Object of research
 - Sandia Flame D (*Sandia National Laboratories, CA, USA*)
- Experimental data
 - High-precision laser measurements
 - Mean and root-mean-square (RMS) profiles of temperature, velocity components, concentrations of 9 major species
 - Axial and 8 radial profiles



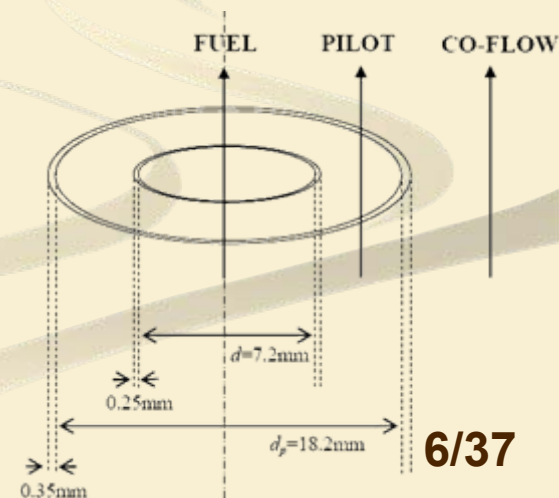
Problem description

Sandia Flame D

- Jet flame with pilot-stabilizer
- Premixed methane-air mixture
 - Highly reduced pollutant formation
 - Accurate experimental measurement
 - Avoiding flame extinction
- Fully developed turbulence

Reynolds number, based on jet speed

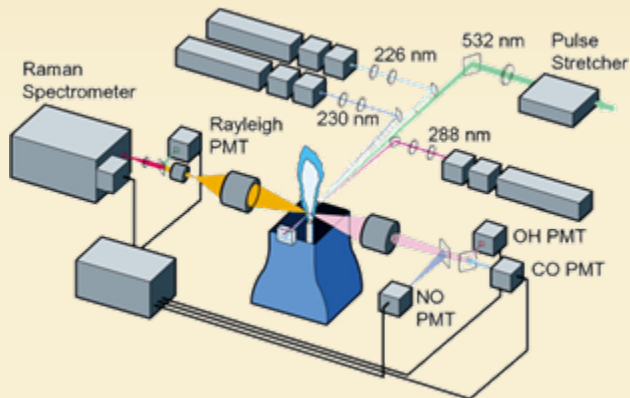
$Re=22400$



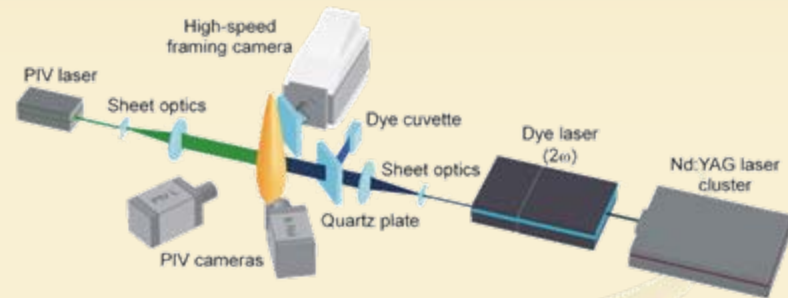
Problem description

High-precision laser measurements

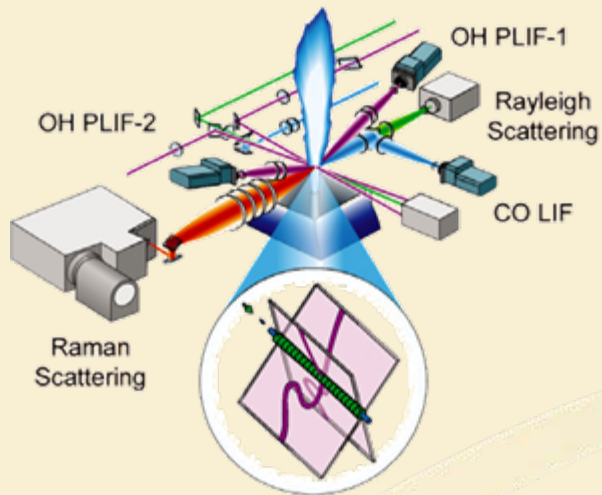
Raman spectrometry



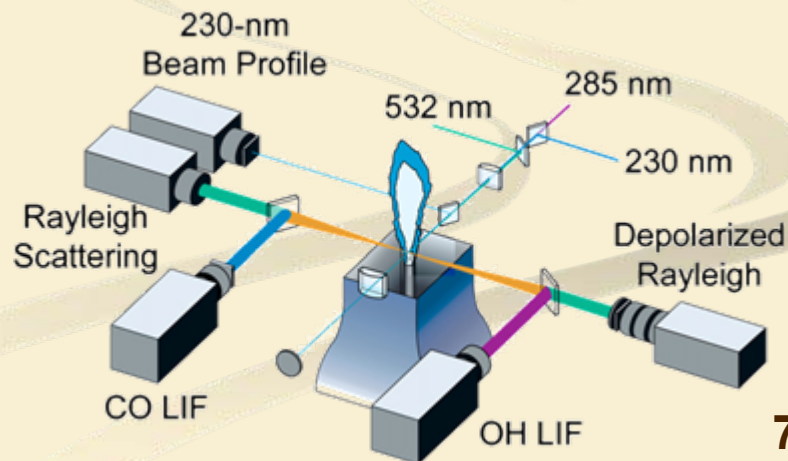
PIV measurements



LIF & PLIF spectrometry

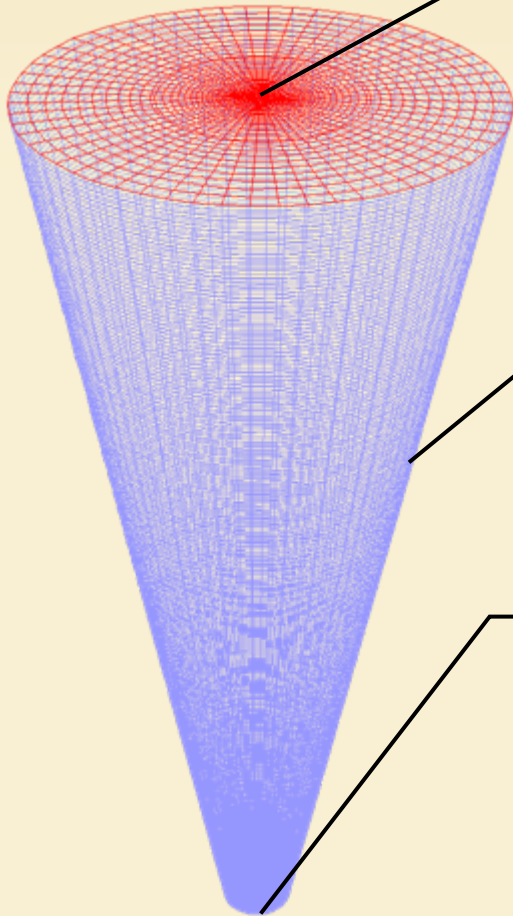


CO, OH LIF measurements



Problem statement

Problem domain and boundary conditions



Defined:

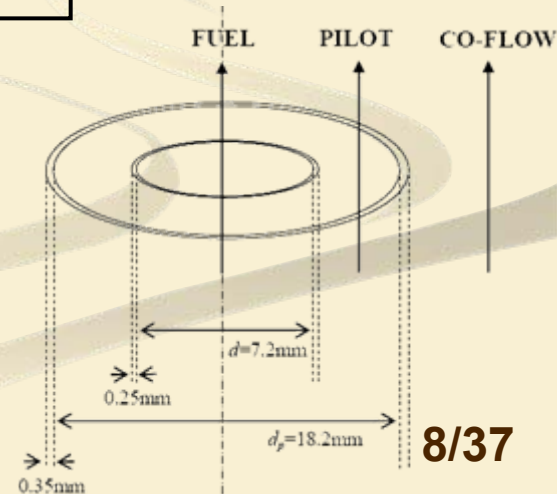
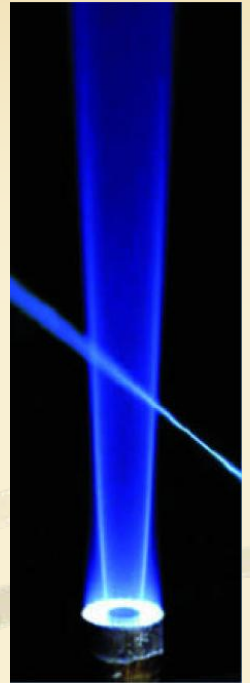
- Pressure
- Backflow parameters

Defined:

- Velocity
- Temperature
- Turbulence
- Mixture composition

Defined:

- Velocity
- Temperature
- Turbulence
- Mixture composition



Mathematical model

Favre-average (filtered) Navier-Stokes equations for multicomponent reacting medium

Continuity equation:

$$\frac{\partial \bar{\rho}}{\partial t} + \frac{\partial \bar{\rho} \tilde{u}_j}{\partial x_j} = 0$$

Momentum transport equation:

$$\frac{\partial \bar{\rho} \tilde{u}_i}{\partial t} + \frac{\partial \bar{\rho} \tilde{u}_j \tilde{u}_i}{\partial x_j} = - \frac{\partial \bar{\rho} \tilde{u}_j'' u_i''}{\partial x_j} - \frac{\partial \bar{P}}{\partial x_j} - \frac{\partial \bar{\tau}_{ij}}{\partial x_j} + \bar{\rho} g_i$$

Species transport equation:

$$\frac{\partial \bar{\rho} \tilde{Y}_\alpha}{\partial t} + \frac{\partial \bar{\rho} \tilde{u}_j \tilde{Y}_\alpha}{\partial x_j} = - \frac{\partial \bar{\rho} \tilde{u}_j'' Y_\alpha''}{\partial x_j} - \frac{\partial \bar{F}_{j,\alpha}}{\partial x_j} + \bar{\dot{r}}_\alpha$$

Enthalpy transport equation:

$$\frac{\partial \bar{\rho} \tilde{h}}{\partial t} + \frac{\partial \bar{\rho} \tilde{u}_j \tilde{h}}{\partial x_j} = \frac{\partial \bar{P}}{\partial t} - \frac{\partial \bar{\rho} \tilde{u}_j'' h''}{\partial x_j} - \frac{\partial}{\partial x_j} \left(\bar{F}_{j,h} + \overline{u_j \tau_{ij}} \right) - \frac{\partial \bar{q}_j^r}{\partial x_j} + \overline{\rho u_i g_i}$$

RANS Turbulence models:

- k-ε Standard
- k-ε RNG
- k-ε Realizable
- k-ω Standard
- k-ω SST
- RSM Linear
- RSM Quadratic
- RSM Low Reynolds

LES Smagorinsky

Mathematical model

Favre-average (filtered) Navier-Stokes equations for multicomponent reacting medium

Continuity equation:

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Momentum transport equation:

$$\frac{\partial \bar{\rho} \tilde{u}_i}{\partial t} + \frac{\partial \bar{\rho} \tilde{u}_j \tilde{u}_i}{\partial x_j} = - \frac{\partial \bar{\rho} u''_j u''_i}{\partial x_j} - \frac{\partial \bar{P}}{\partial x_j} - \frac{\partial \bar{\tau}_{ij}}{\partial x_j} + \bar{\rho} g_i$$

Species transport equation:

$$\frac{\partial \bar{\rho} \tilde{Y}_\alpha}{\partial t} + \frac{\partial \bar{\rho} \tilde{u}_j \tilde{Y}_\alpha}{\partial x_j} = - \frac{\partial \bar{\rho} u''_j Y''_\alpha}{\partial x_j} - \frac{\partial \bar{F}_{j,\alpha}}{\partial x_j} + \bar{\dot{r}}_\alpha$$

Enthalpy transport equation:

$$\frac{\partial \bar{\rho} \tilde{h}}{\partial t} + \frac{\partial \bar{\rho} \tilde{u}_j \tilde{h}}{\partial x_j} = \frac{\partial \bar{P}}{\partial t} - \frac{\partial \bar{\rho} u''_j h''}{\partial x_j} - \frac{\partial}{\partial x_j} \left(\bar{F}_{j,h} + \overline{u_i \tau_{ij}} \right) - \frac{\partial \bar{q}_j^r}{\partial x_j} + \overline{\rho u_i g_i}$$

Chemistry models:

- Eddy Break-up model (*EBU*)
- Mixture fraction based statistical model (*PDF*)

Radiation models:

- Discrete transfer
- Discrete ordinates

Mathematical model

Turbulence models

- **Family of k - ε turbulence models**
Turbulent kinetic energy and its dissipation rate
- **Family of k - ω turbulence models**
Turbulent kinetic energy and specific dissipation rate
- **Family of Reynolds Stress models**
Six turbulent stresses separately
- **Large Eddy Simulation model**
Subgrid turbulence models without additional equations

$$\frac{\partial \bar{\rho}(\cdot)}{\partial t} + \frac{\partial \bar{\rho} \tilde{u}_j(\cdot)}{\partial x_j} = \underbrace{\frac{\partial}{\partial x_j} (\dots)}_{\text{Diffusion}} - \underbrace{(\dots)}_{\text{Production}} - \underbrace{(\dots)}_{\text{Dissipation}}$$

Mathematical model

Chemistry models

- Eddy Break-up model

Fast chemistry assumption (infinitely fast reactions)

$$\tilde{r}_a = A\bar{\rho} \frac{\varepsilon}{k} \min\left(\tilde{Y}_{fuel}, \frac{\tilde{Y}_{ox}}{S_{ox}}, B \frac{\tilde{Y}_{prod}}{1 + S_{ox}}\right)$$

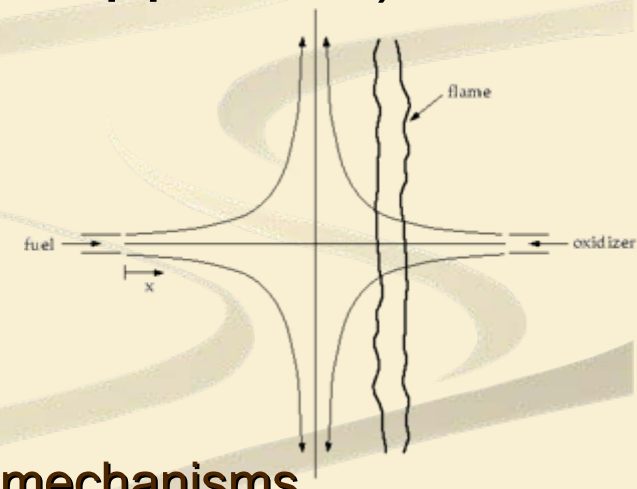
- Statistical model (mixture fraction approach)

- Equilibrium chemistry

Incapability of predicting slow chemistry

- Flamelet models

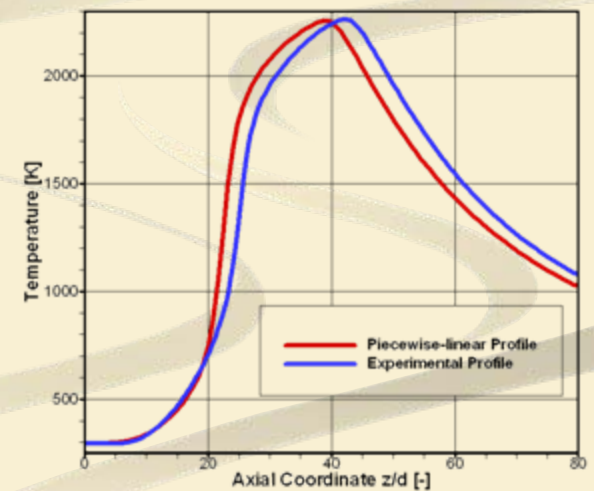
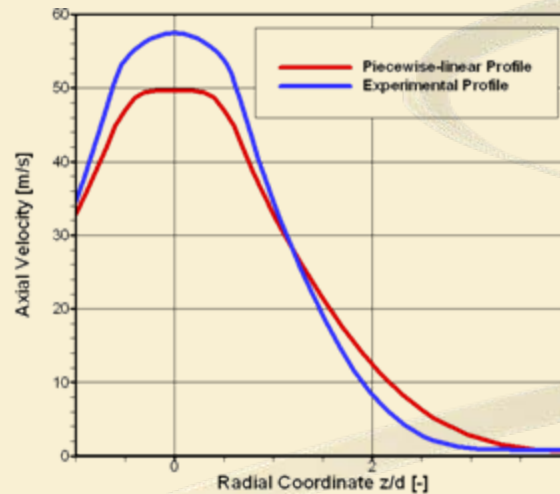
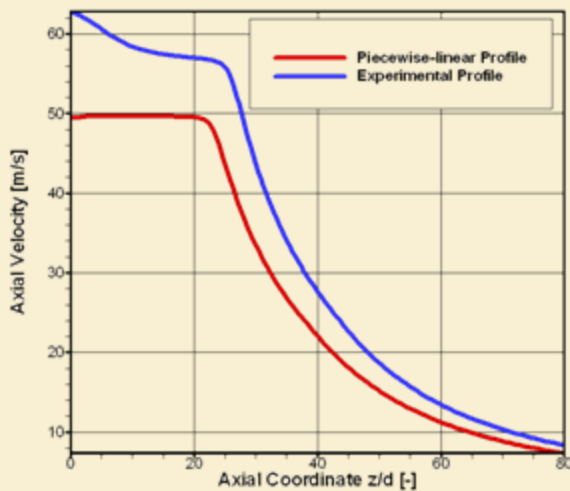
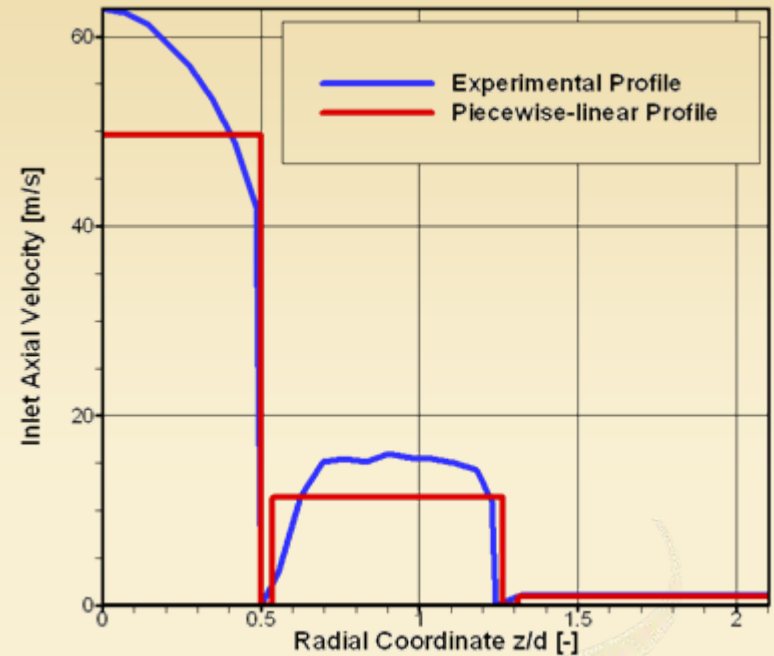
- Thin flame assumption
- Large-scale curvature of flame
- Capability of using detailed chemistry mechanisms



Test simulations

Inlet boundary profile impact

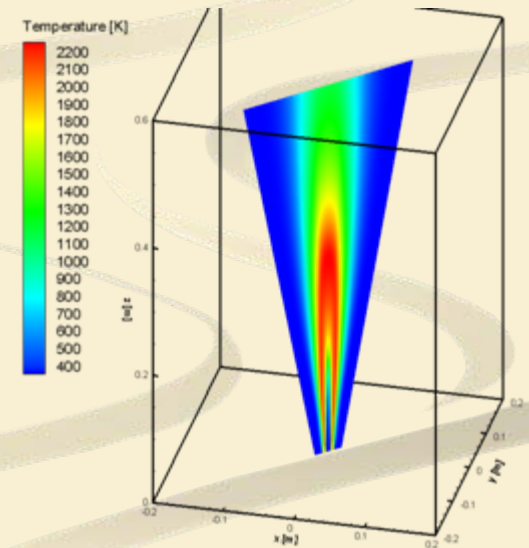
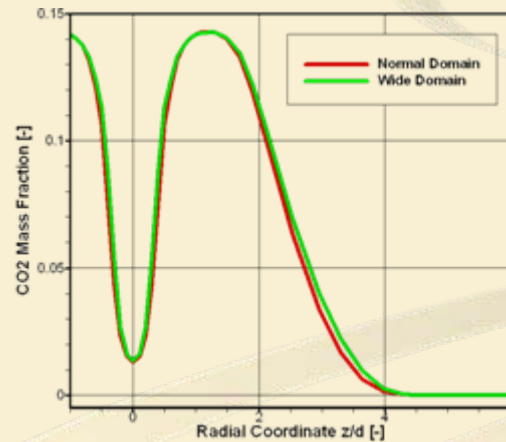
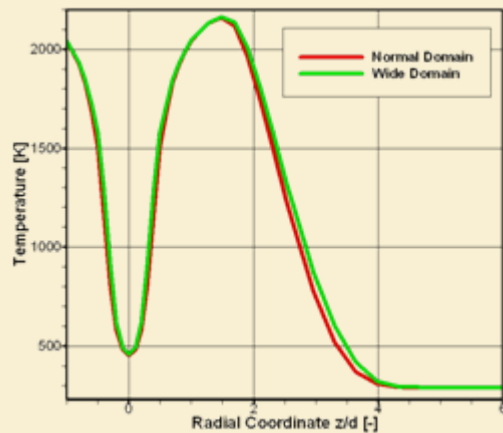
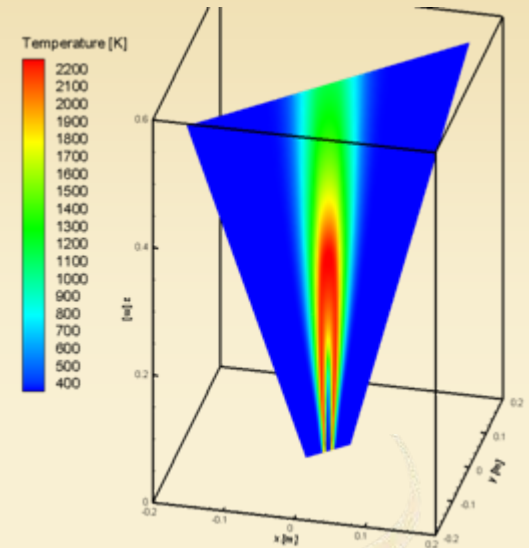
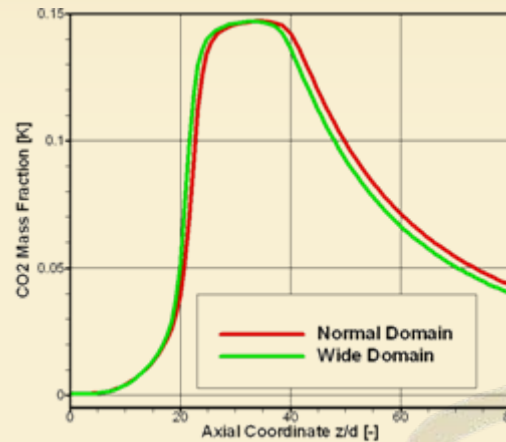
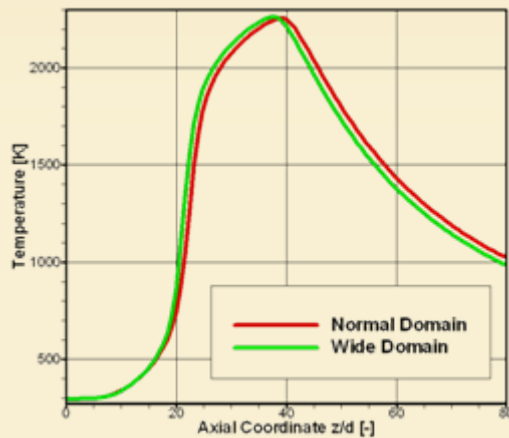
- Velocity experimental profile seriously affects the flame
- Scalar experimental boundary profile impact on the flame is negligible



Test simulations

Domain dimensions impact

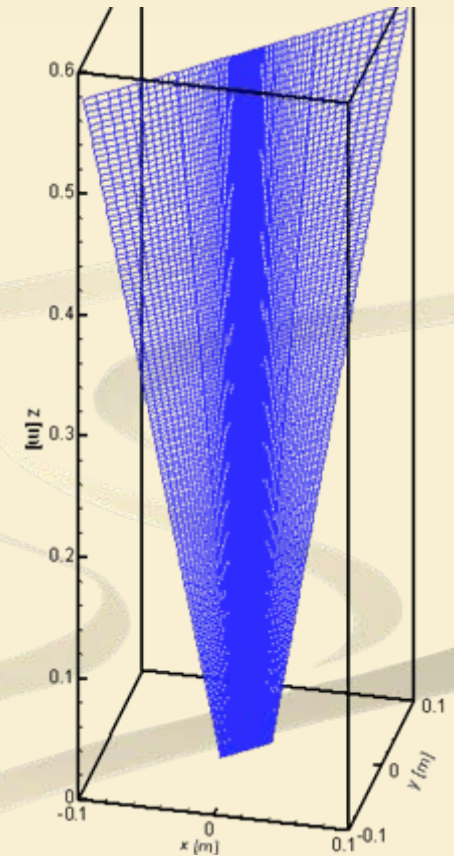
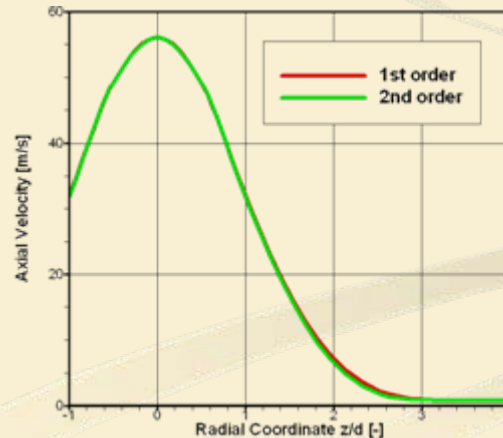
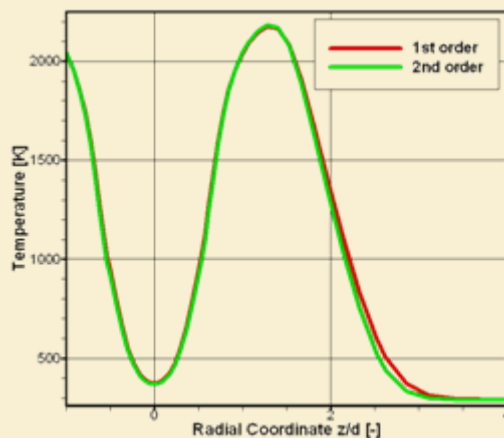
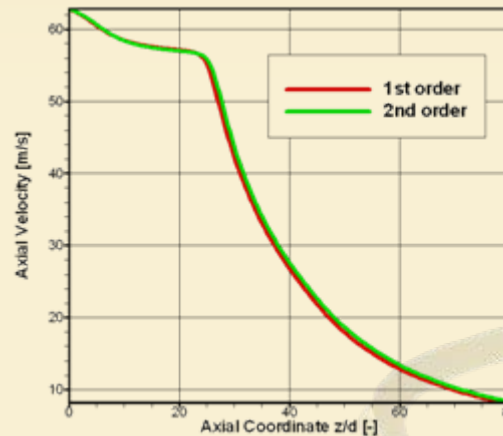
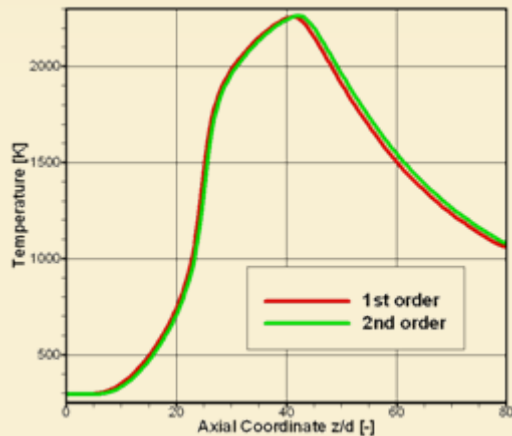
- Domain widening is unreasonable



Test simulations

Approximation order impact

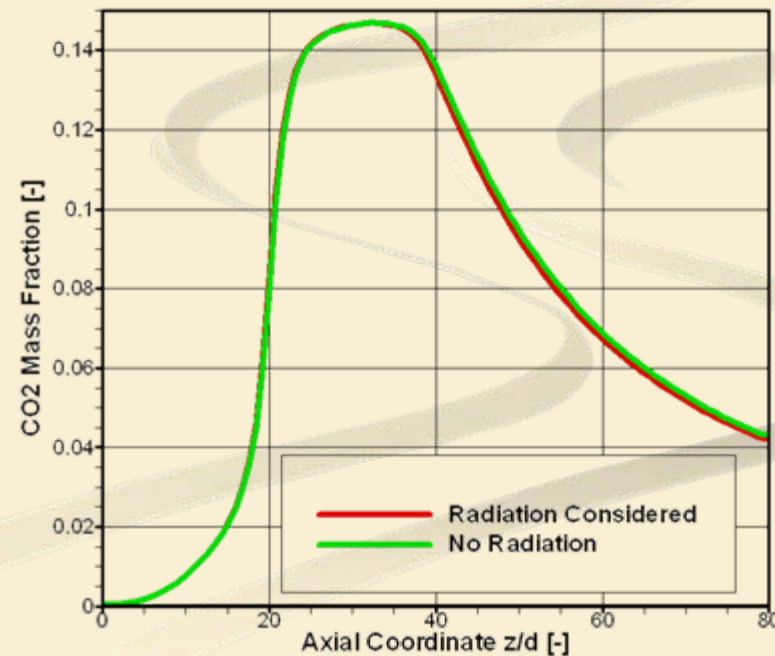
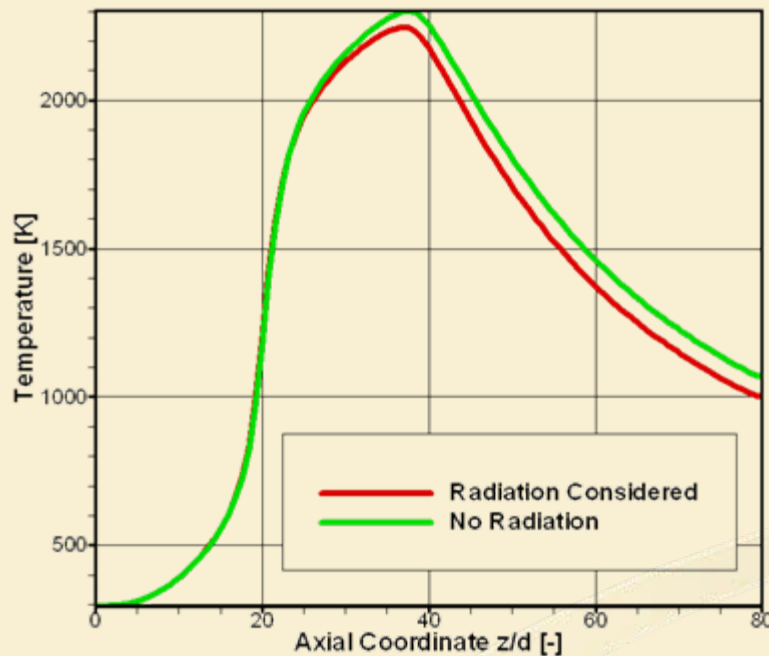
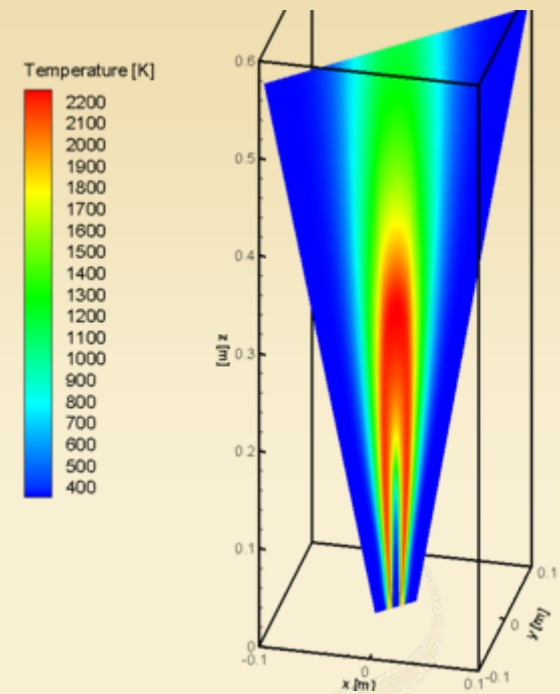
- Discretization order does not seriously affect physical fields
- Still 2-nd order discretization will be used further



Test simulations

Radiation impact

- Radiation consideration affects only temperature field (*100 K* higher peak value)
- Scalar fields are not seriously affected by radiation
- Radiation was considered in all simulations



Simulation results

Turbulence and chemistry modeling strategies:

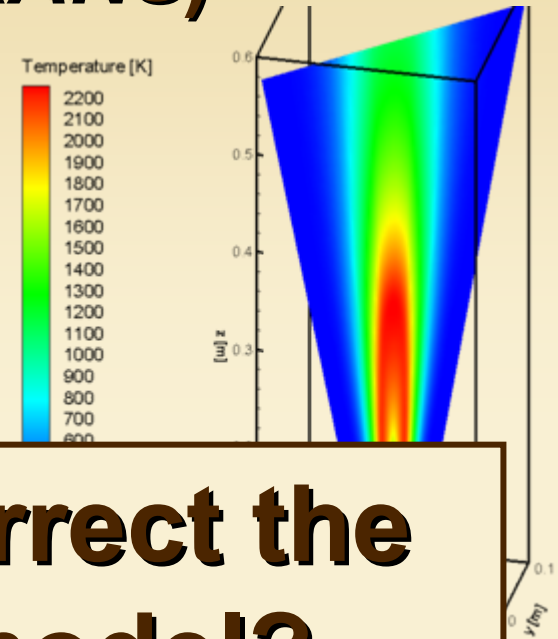
	Favre time-averaging (<i>RANS</i>)	Large eddy simulation (<i>LES</i>)
Eddy break-up model (<i>EBU</i>)	<input checked="" type="checkbox"/> (8x2)	<input checked="" type="checkbox"/> (1x1)
Statistical model (<i>PDF</i>)	<input checked="" type="checkbox"/> (8x4)	<input checked="" type="checkbox"/> (1x1)

+ Accounting for radiation

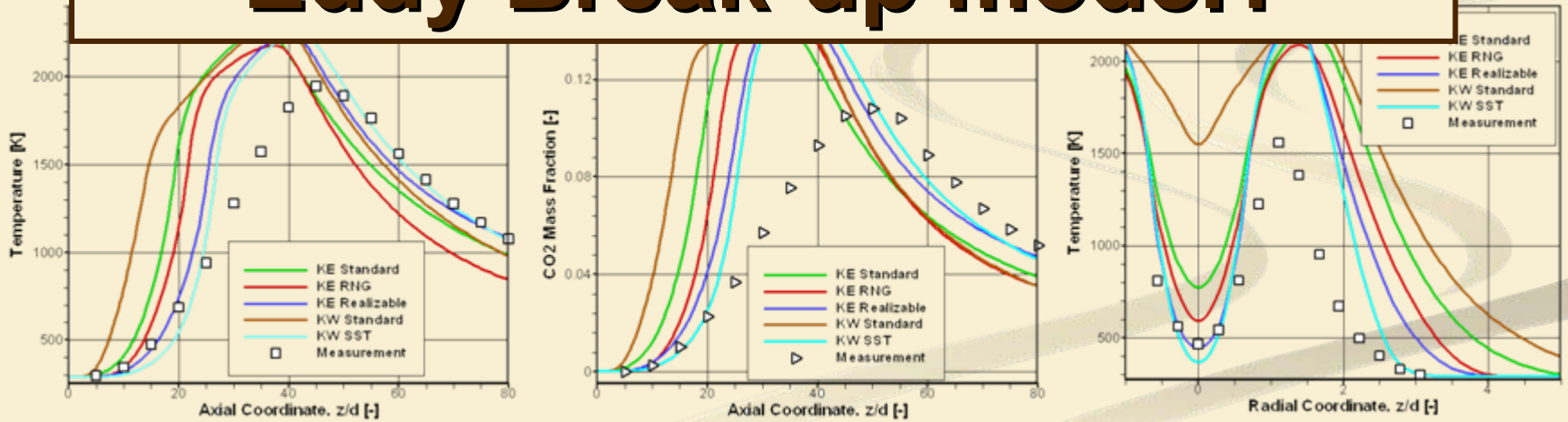
Reynolds time-averaging (RANS)

Chemistry: Eddy Break-up model

- Peak temperatures are greatly overestimated (about 300 K)
- Peak concentrations of reaction products are greatly overestimated (about 15-40%)



Is it possible to correct the Eddy Break-up model?



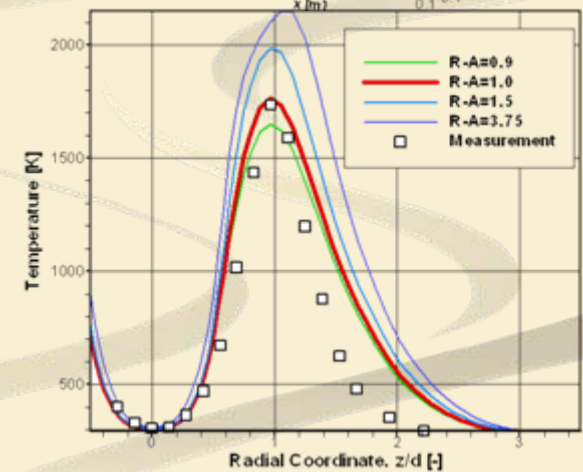
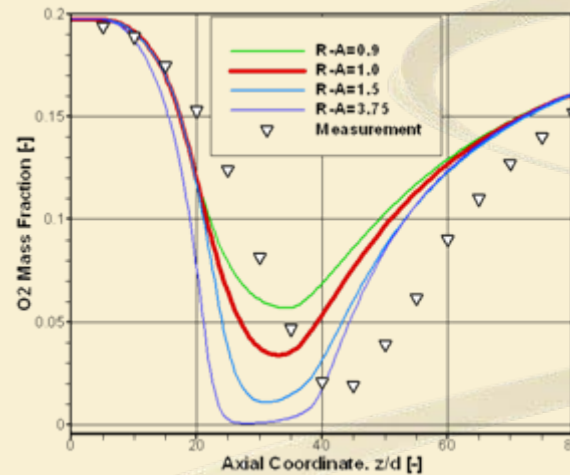
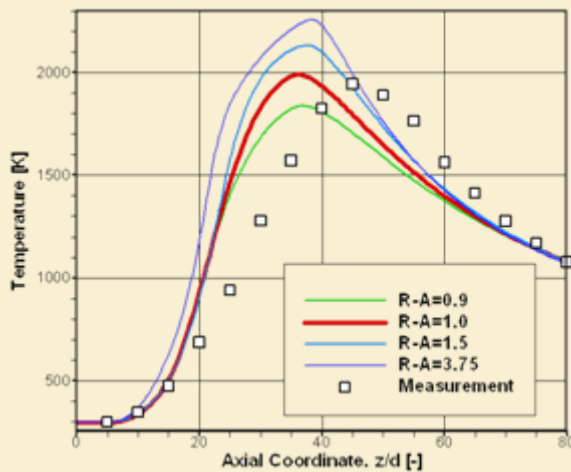
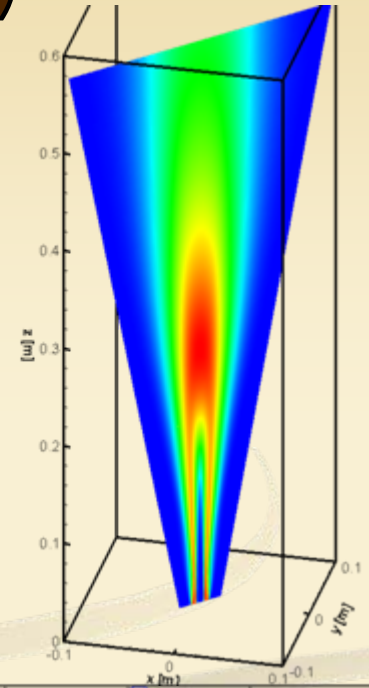
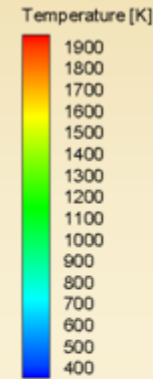
Reynolds time-averaging (RANS)

Eddy Break-up model improvement

- Generally accepted value of A -constant is 4.0

$$\tilde{\tau}_a = A \bar{\nu} \frac{\varepsilon}{k} \min \left(\tilde{Y}_{fuel}, \frac{\tilde{Y}_{ox}}{S_{ox}}, B \frac{\tilde{Y}_{prod}}{1 + S_{ox}} \right)$$

- Optimal constant value is $A=1.0$
- Significant variation of constant means poor model adaptability to different types of reacting flows



Theory interlude

Chemistry: statistical model

Transport equation for α -specie:

$$\frac{\partial \rho Y_\alpha}{\partial t} + \frac{\partial \rho u_j Y_\alpha}{\partial x_j} = -\frac{\partial F_{j,\alpha}}{\partial x_j} + \dot{r}_\alpha$$

Combining different equations:

$$\frac{\partial \rho (Y_{fuel} - Y_\alpha / s_\alpha)}{\partial t} + \frac{\partial \rho u_j (Y_{fuel} - Y_\alpha / s_\alpha)}{\partial x_j} - \frac{\partial}{\partial x_j} \rho \mathcal{D}_\alpha \frac{\partial (Y_{fuel} - Y_\alpha / s_\alpha)}{\partial x_j} = 0$$

Mixture fraction is a concrete conserved scalar:

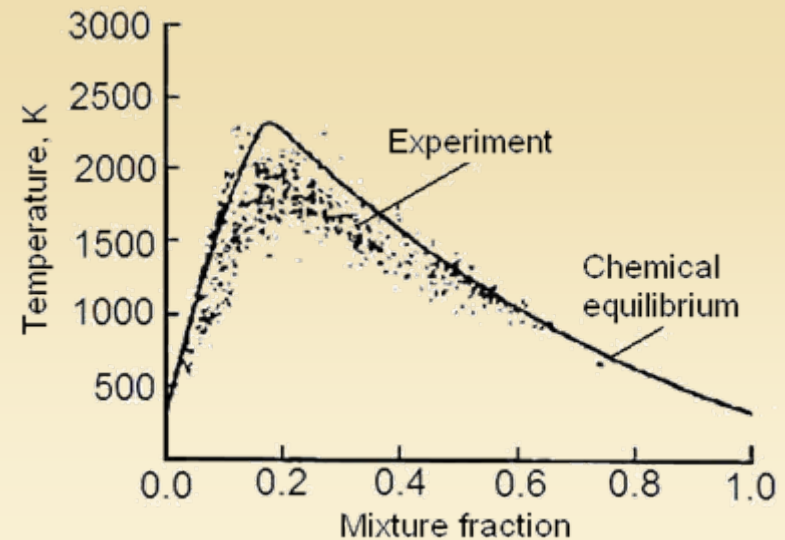
$$Z = \frac{Y_{fuel} - Y_{ox} / s_{ox} - (Y_{fuel}^{air} - Y_{ox}^{air} / s_{ox})}{Y_{fuel}^{fl} - Y_{ox}^{fl} / s_{ox} - (Y_{fuel}^{air} - Y_{ox}^{air} / s_{ox})}$$

Using equilibrium dependencies:

$$Y_\alpha = Y_\alpha(Z) \quad T = T(Z) \quad \rho = \rho(Z)$$

Averaged quantities with B -function as density function:

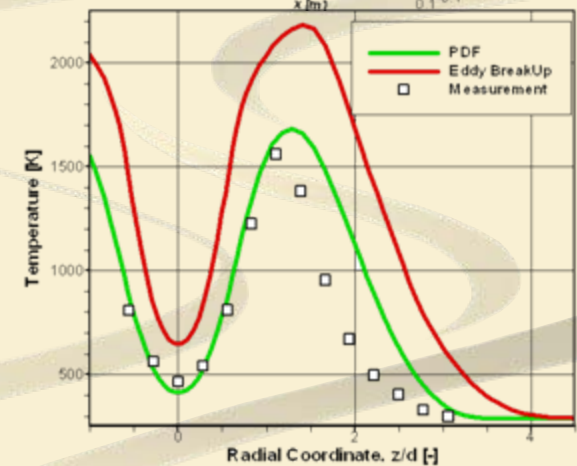
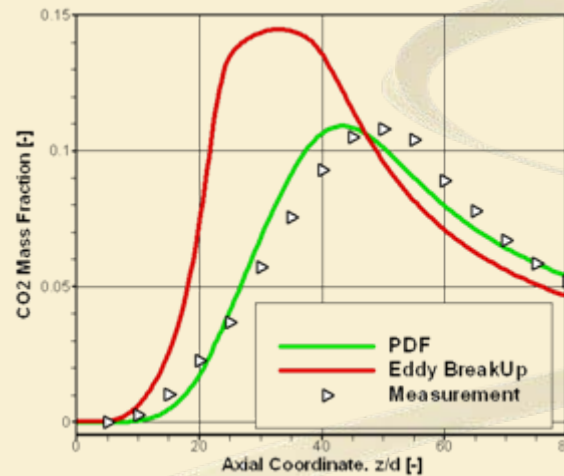
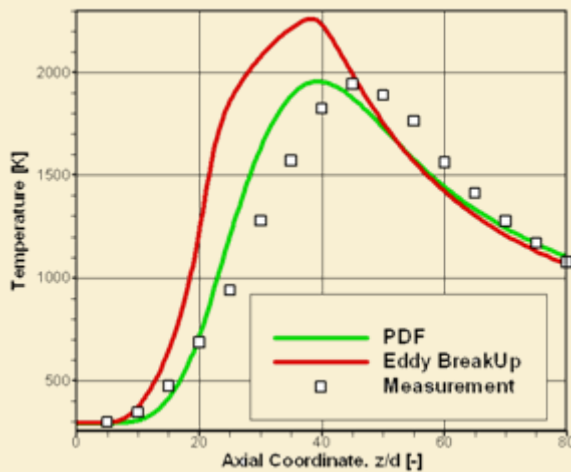
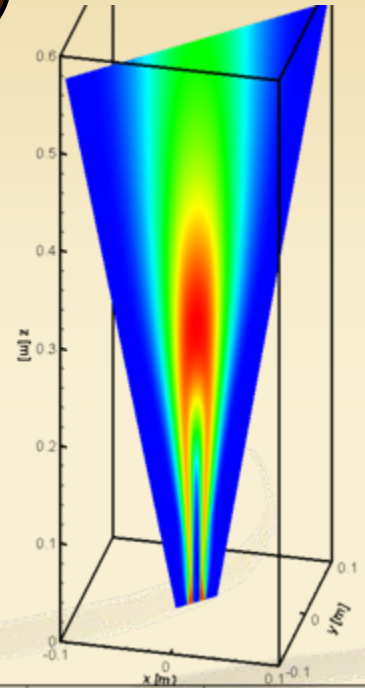
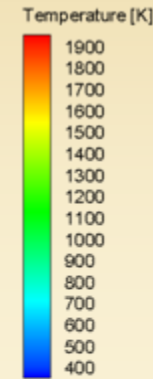
$$\tilde{Y}_\alpha = \int_0^1 Y_\alpha(Z) \tilde{P}(Z) dZ \quad \tilde{T} = \int_0^1 T(Z) \tilde{P}(Z) dZ \quad \bar{\rho} = \left(\int_0^1 \rho^{-1}(Z) \tilde{P}(Z) dZ \right)^{-1}$$



Reynolds time-averaging (RANS)

Chemistry: statistical model

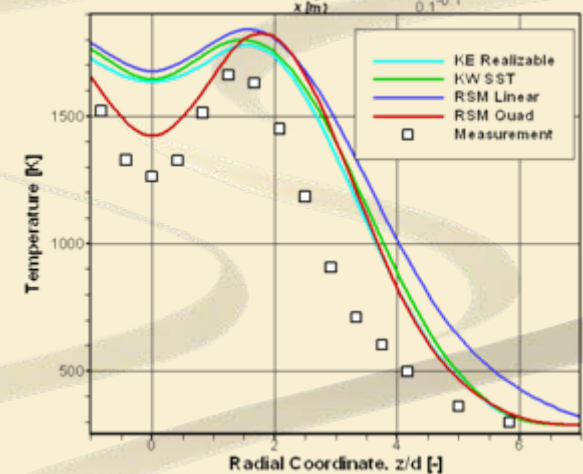
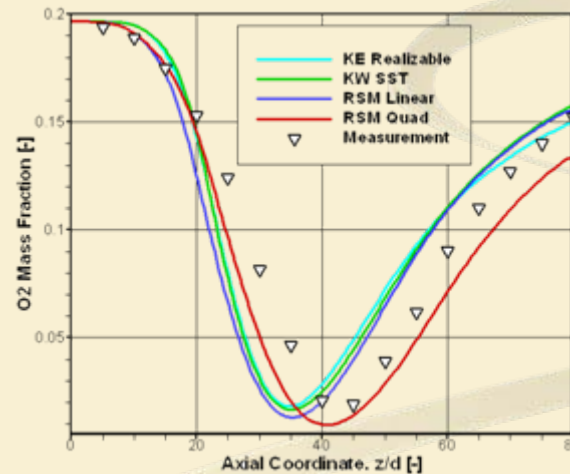
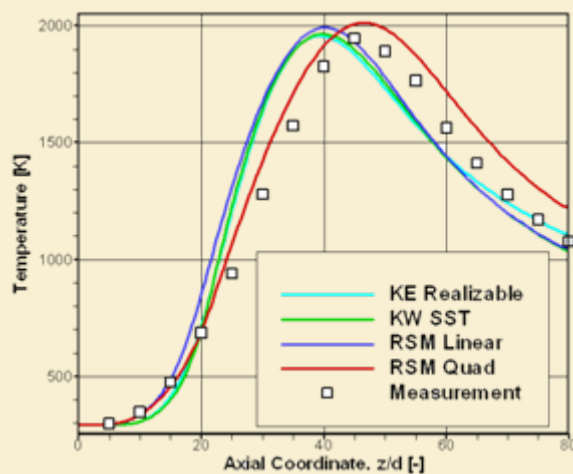
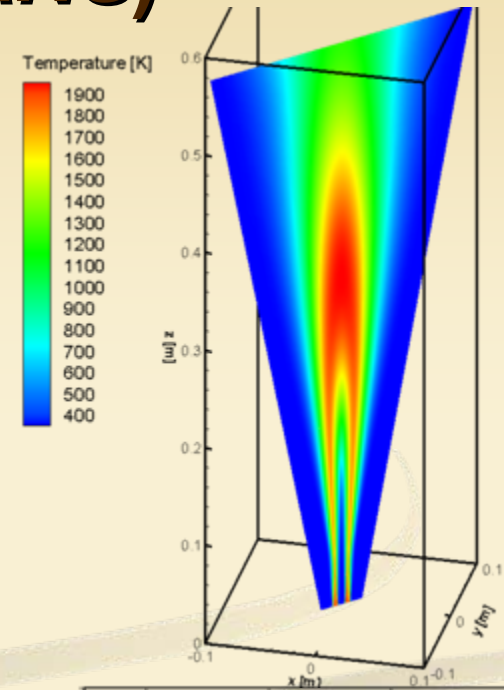
- Significantly more accurate flame prediction
- Correct peak values of temperature and reaction products
- More narrow and long flame than in Eddy Break-up model



Reynolds time-averaging (RANS)

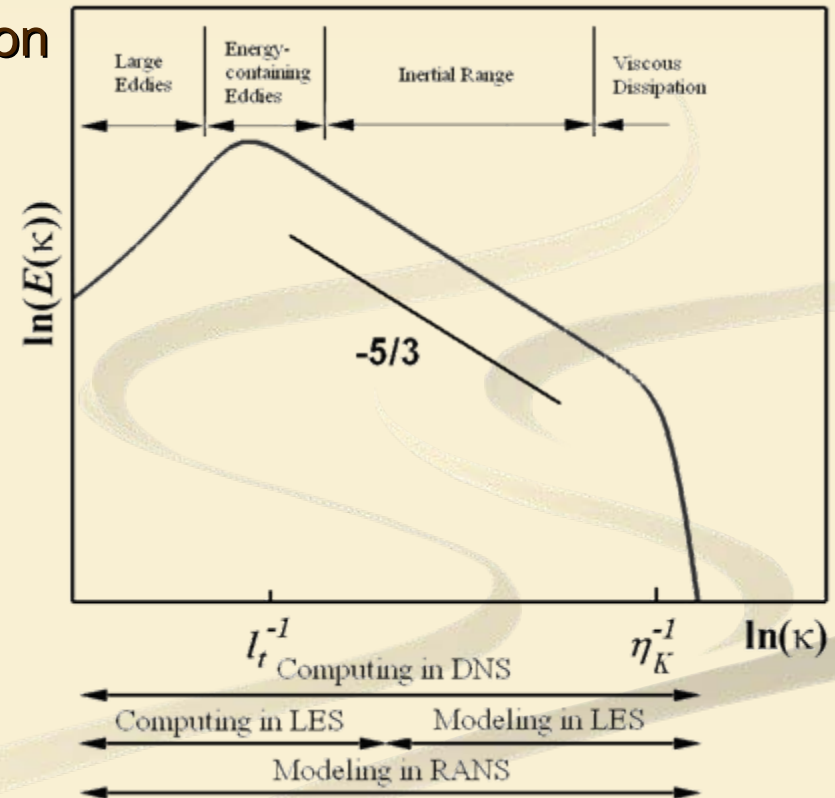
Turbulence models

- Best models with two additional turbulence equations: *k-ε Realizable* and *k-ω SST*
- *Quadratic Reynolds Stress model (RSM)* is the most accurate stationary model
- *k-ε Standard*, *k-ε RNG*, *k-ω Standard*, *RSM LowRe* models are significantly worse

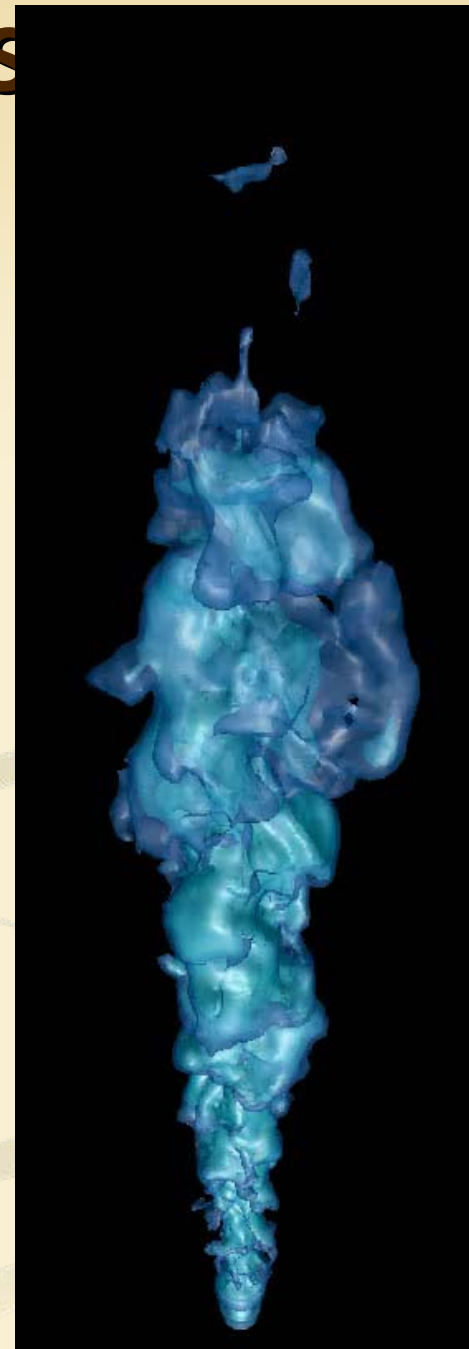
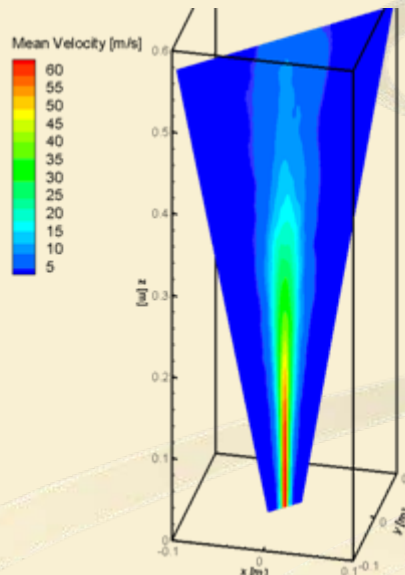
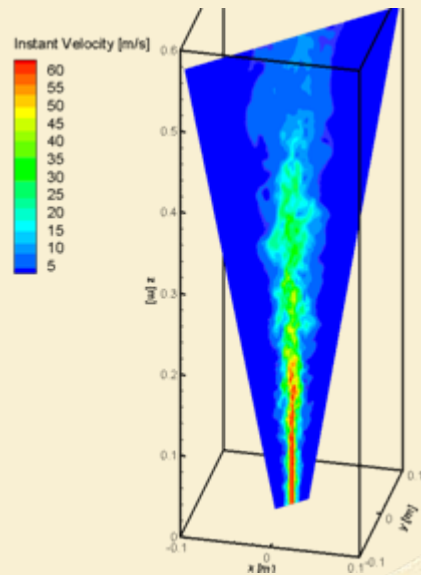
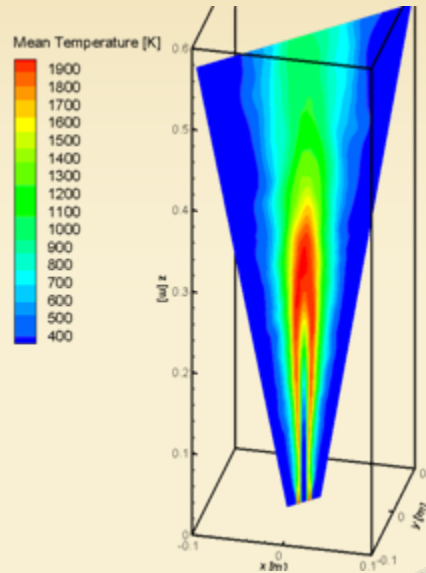
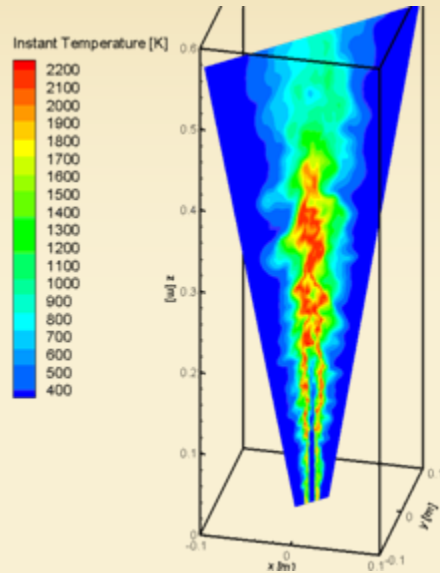


Theory interlude

- Favre time-averaging (*RANS*) is a conventional engineering approach
- Large Eddy Simulation (*LES*) capabilities
 - Less modeling, more calculation
 - Enables explicitly resolve energy-bearing long-wave part of vortex spectrum
 - High computational cost
 - Currently introduces in engineering practice



Large Eddy Simulation (LES)



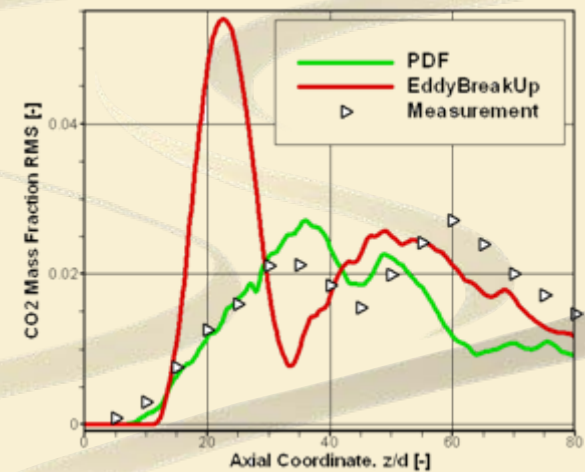
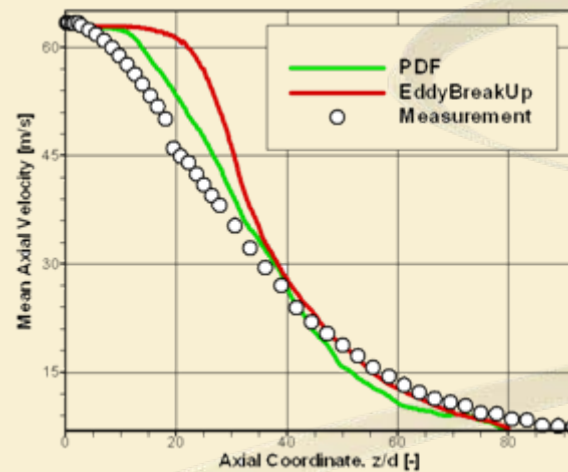
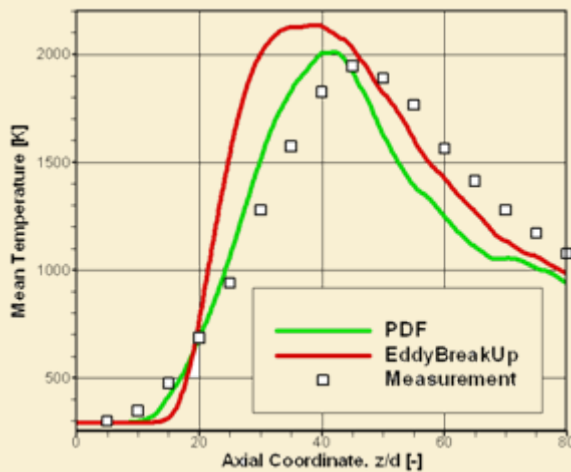
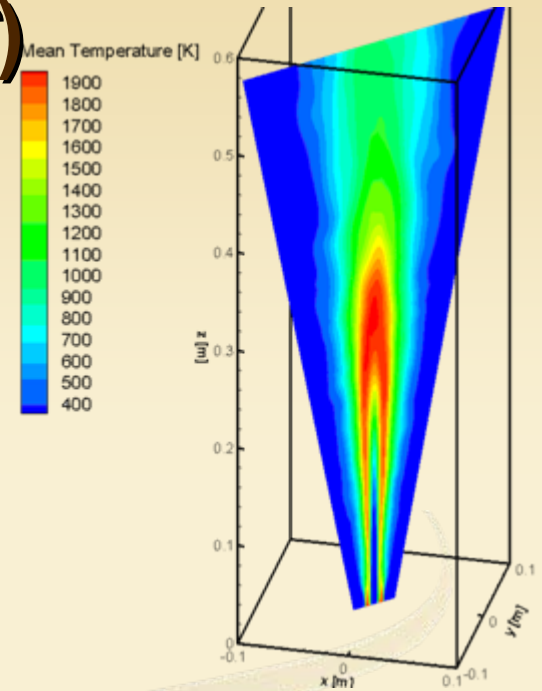
Large Eddy Simulation (LES)

Chemistry model

- Eddy Break-up model for *LES* is more accurate than Eddy Break-up model for *RANS*

$$\tilde{\tau}_a = A \bar{\rho} \tau^{\gamma} \min \left(\tilde{Y}_{fuel}, \frac{\tilde{Y}_{ox}}{S_{ox}}, B \frac{\tilde{Y}_{prod}}{1 + S_{ox}} \right) \quad \tau^r = \left(\sqrt{2S_{ij}S_{ij}} \right)^{-1}$$

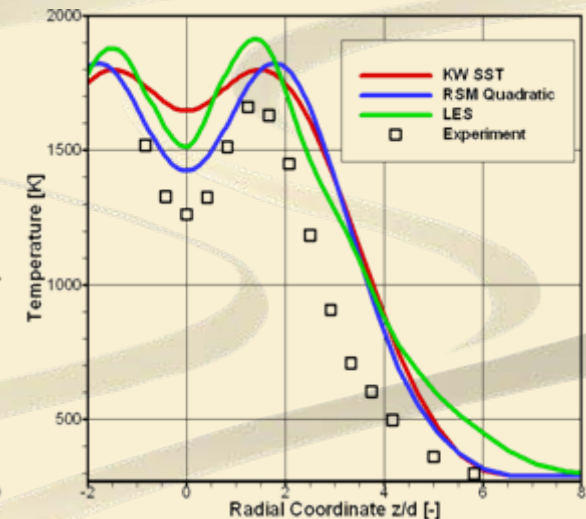
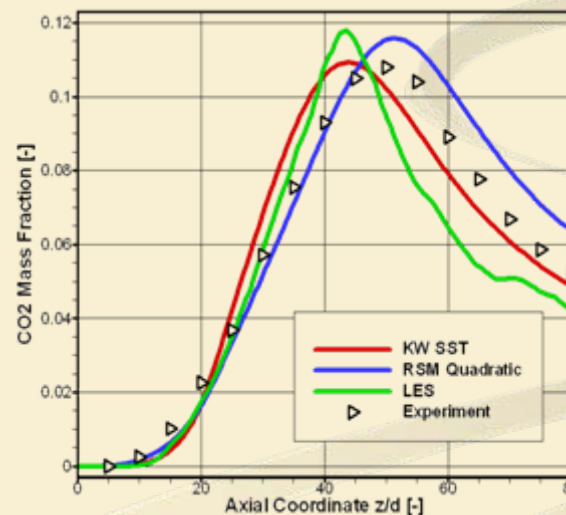
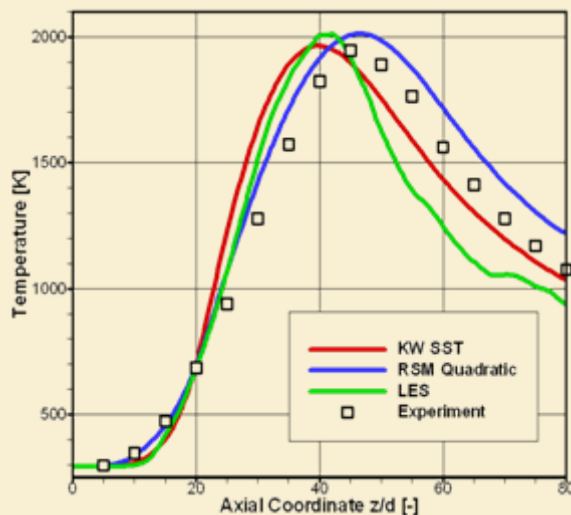
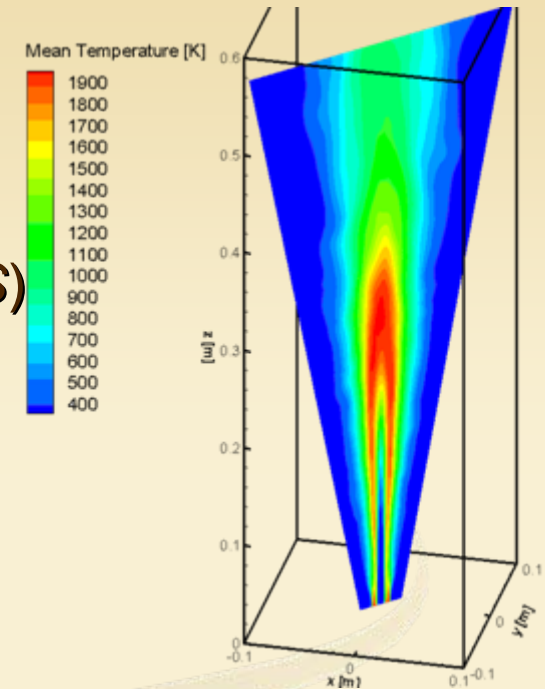
- Statistical model is still preferable
- Good agreement for 2-nd order statistics



Large Eddy Simulation (*LES*)

Turbulence comparison

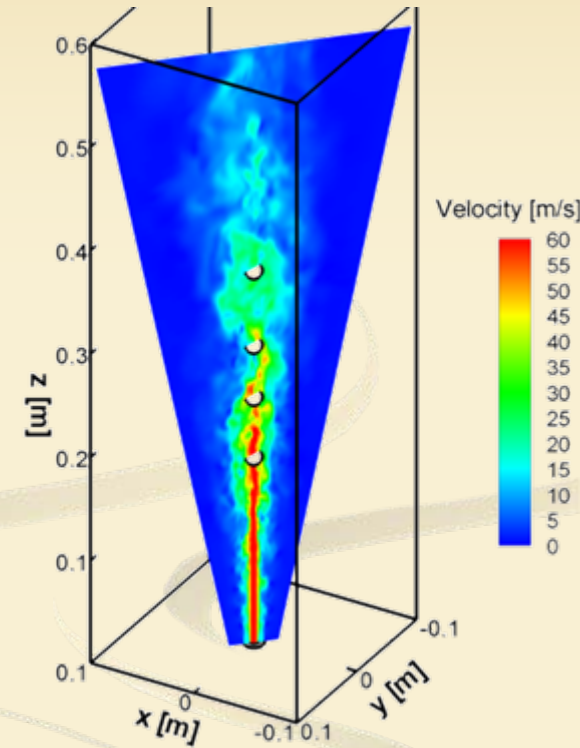
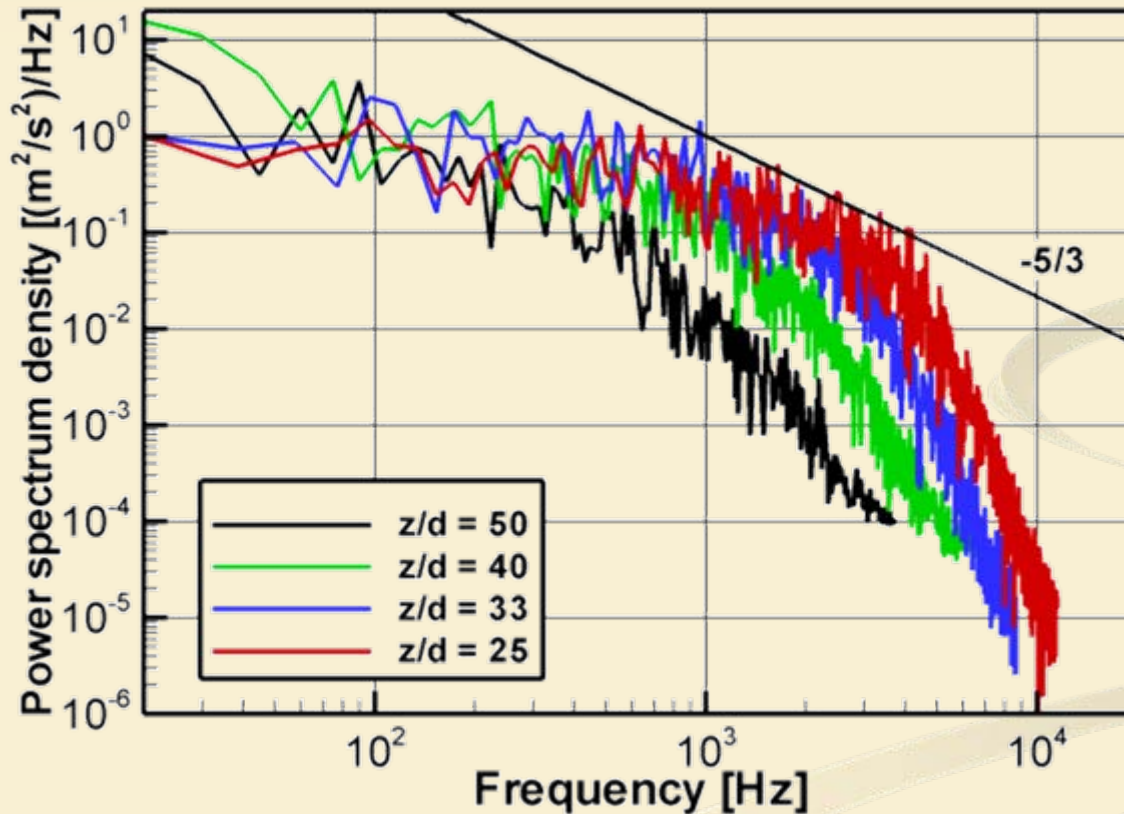
- Perturbations were not generated at inlet (*LES*)
- Good agreement for *LES* up to the peak
- The simplest *LES* model is inferior only to the most comprehensive *RANS* model
- *LES* (as *Quadratic RSM*) predicts correct shape of the flame



Large Eddy Simulation (LES)

Velocity spectrum

- The spectrum $-5/3$ region is captured quite well



Theory interlude

Chemistry: flamelet model

Statistical model complication - flame structure in mixture fraction space

$$\frac{\partial Y_\alpha}{\partial t} = \dot{r}_\alpha(Y_\alpha, T) + \frac{1}{2} \chi \frac{\partial^2 Y_\alpha}{\partial Z^2}$$

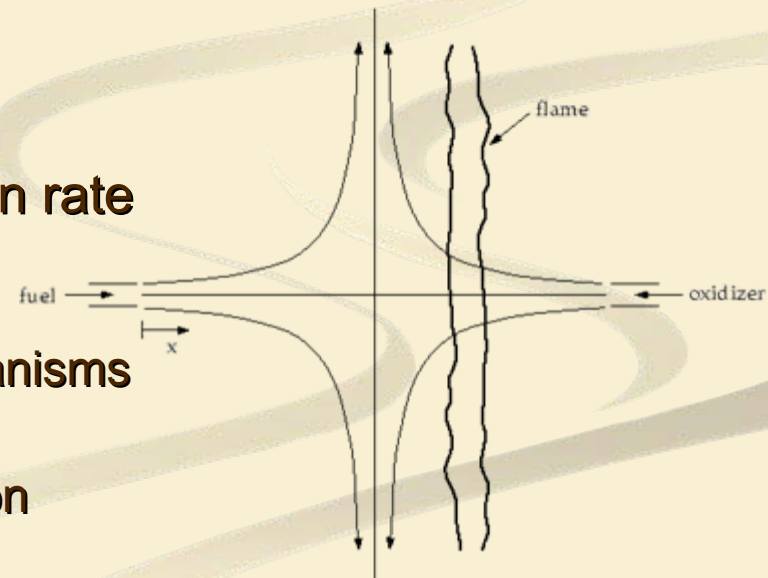
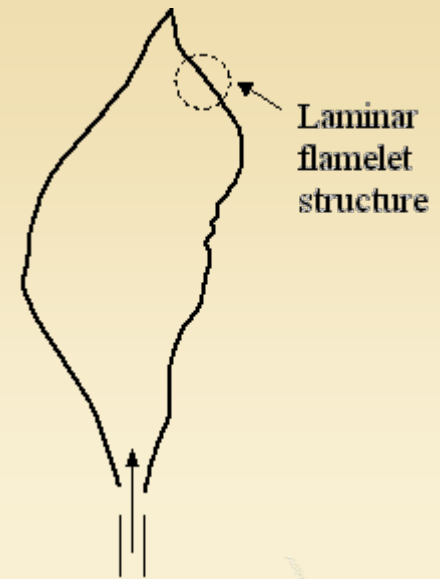
χ - scalar dissipation (parameter)

$$\chi = 2\mathcal{D} \left[\left(\frac{\partial Z}{\partial x_1} \right)^2 + \left(\frac{\partial Z}{\partial x_2} \right)^2 + \left(\frac{\partial Z}{\partial x_3} \right)^2 \right]$$

Scalar dissipation is proportional to strain rate

Characteristics:

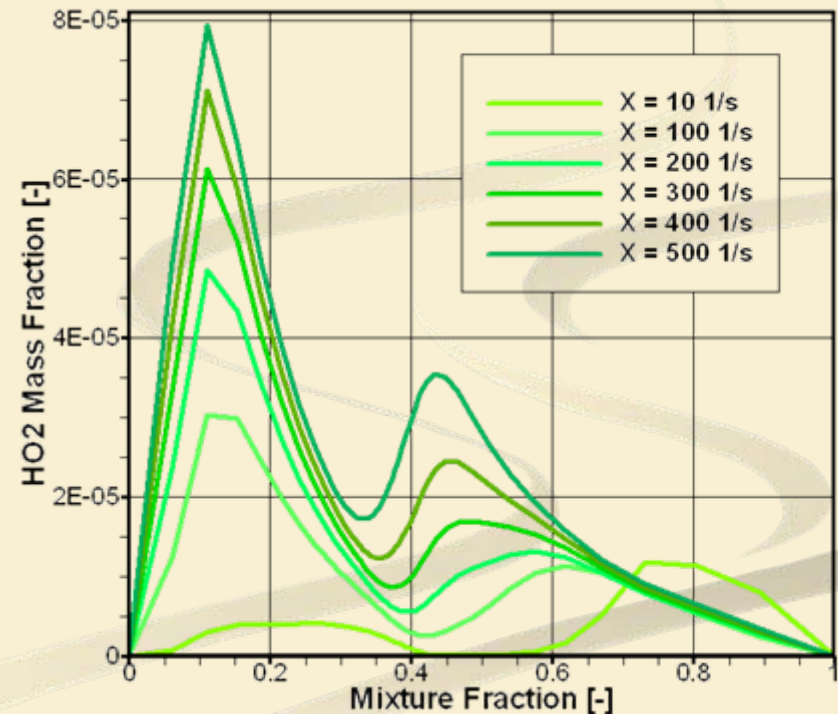
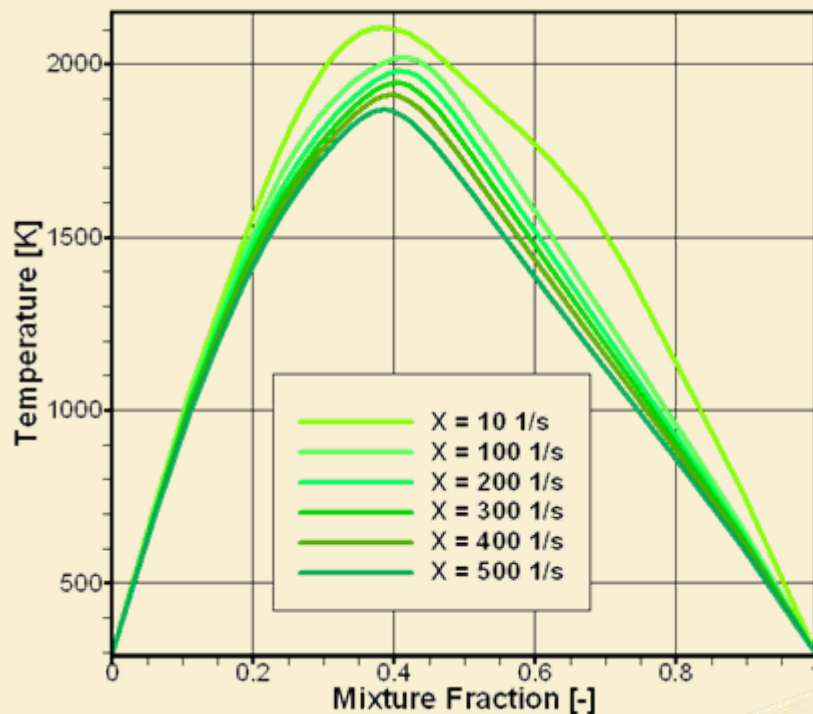
- Capability of using detailed chemistry mechanisms
- Thin flame front assumption
- Fast flame adaptation to flow field assumption



Statistical chemistry

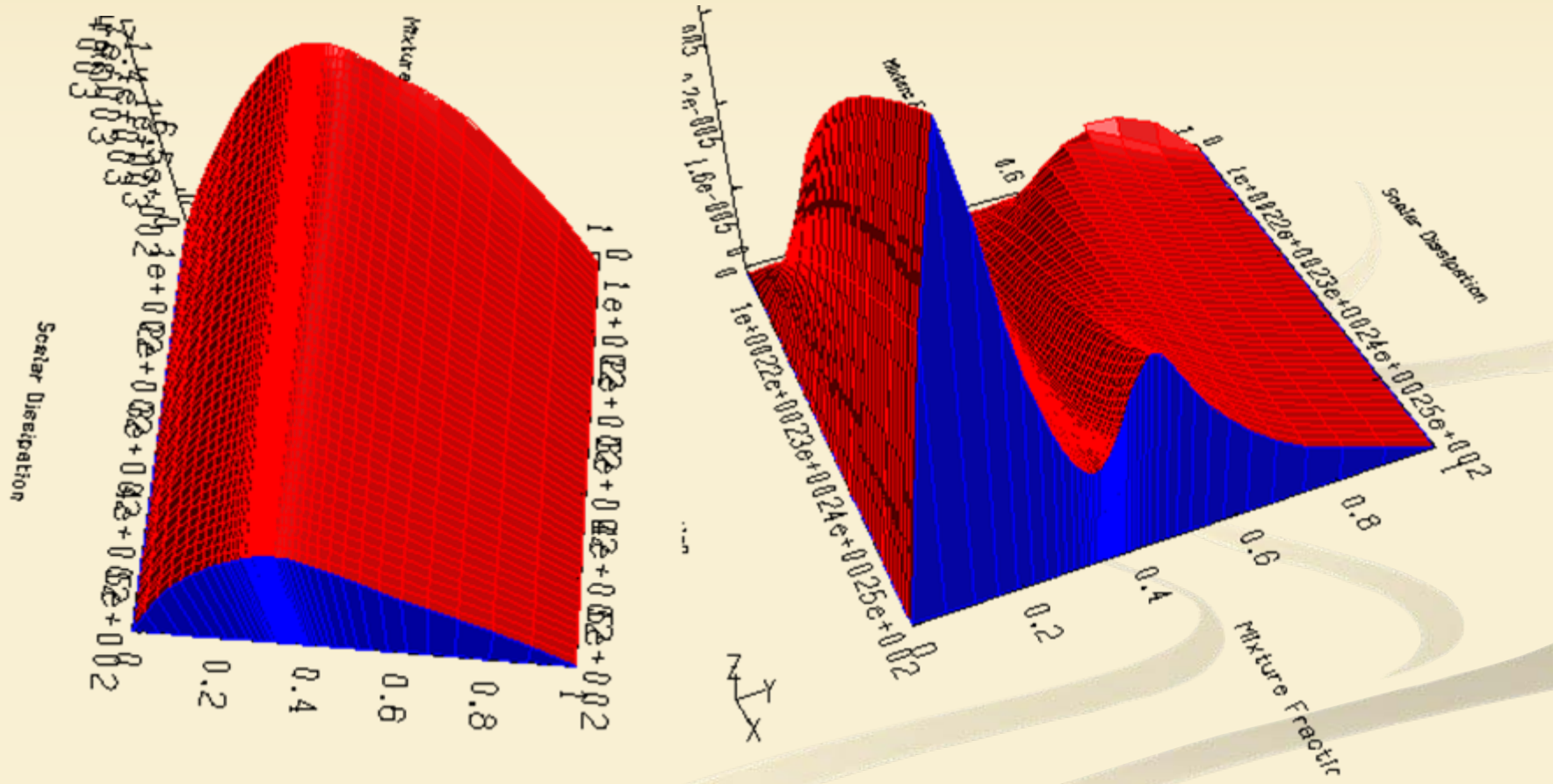
Flamelet construction

- Scalar dissipation does not affect temperature and major species
- Intermediate species are highly scalar-dissipation-dependent
- Still some serious numerical deviations near $\chi = 0$



Statistical chemistry

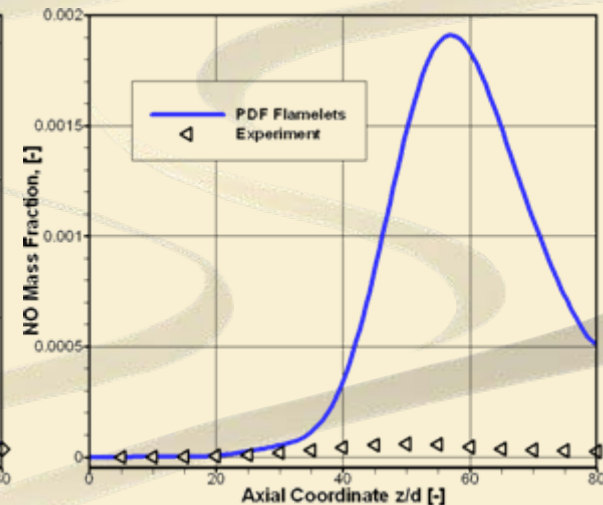
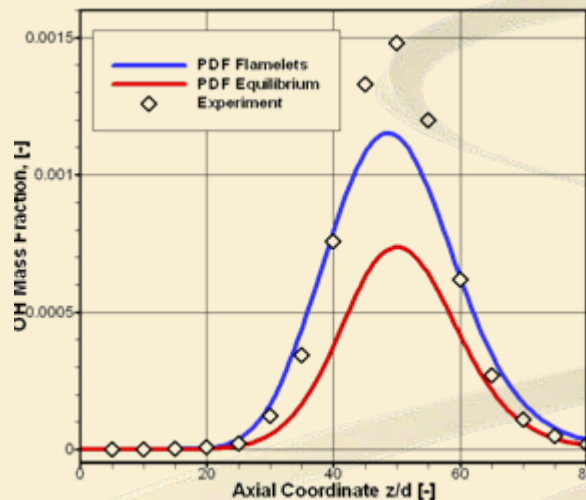
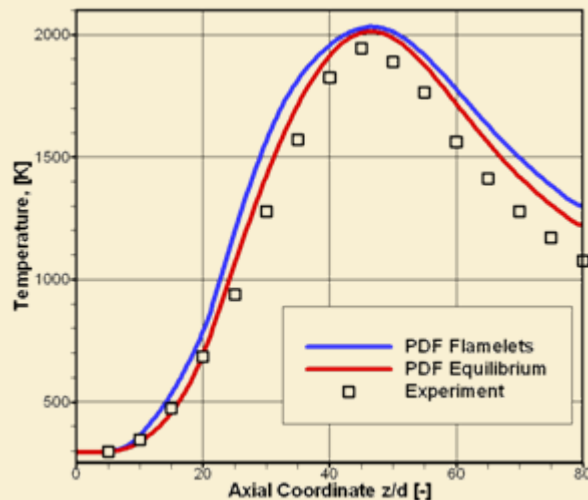
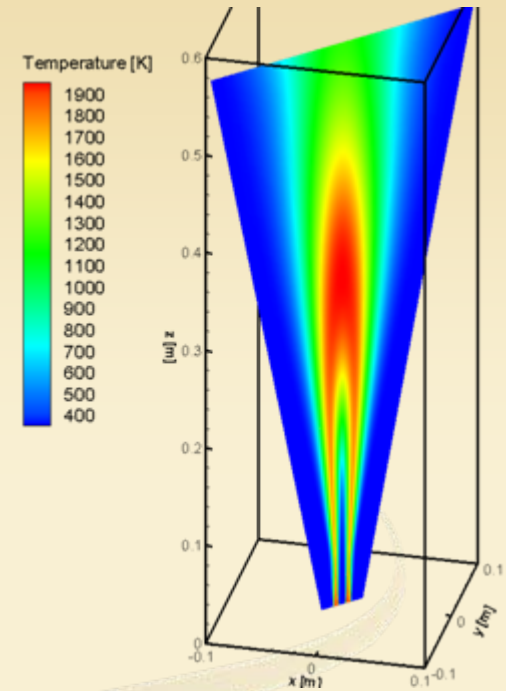
Flamelet construction



Statistical chemistry

Flamelet model

- Flow, scalar and major species fields are quite the same as in Equilibrium chemistry
- Intermediate species fields are significantly improved
- Bad NO field prediction due to specific processes of NO formation



Computational resources



- λ cluster

Cores count:	256 (64 nodes)
Processors:	AMD Opteron 280
Memory:	512 Gb
Network connection:	Infiniband
Peak performance:	1035 GFLOPS
Operating system:	SUSE Linux

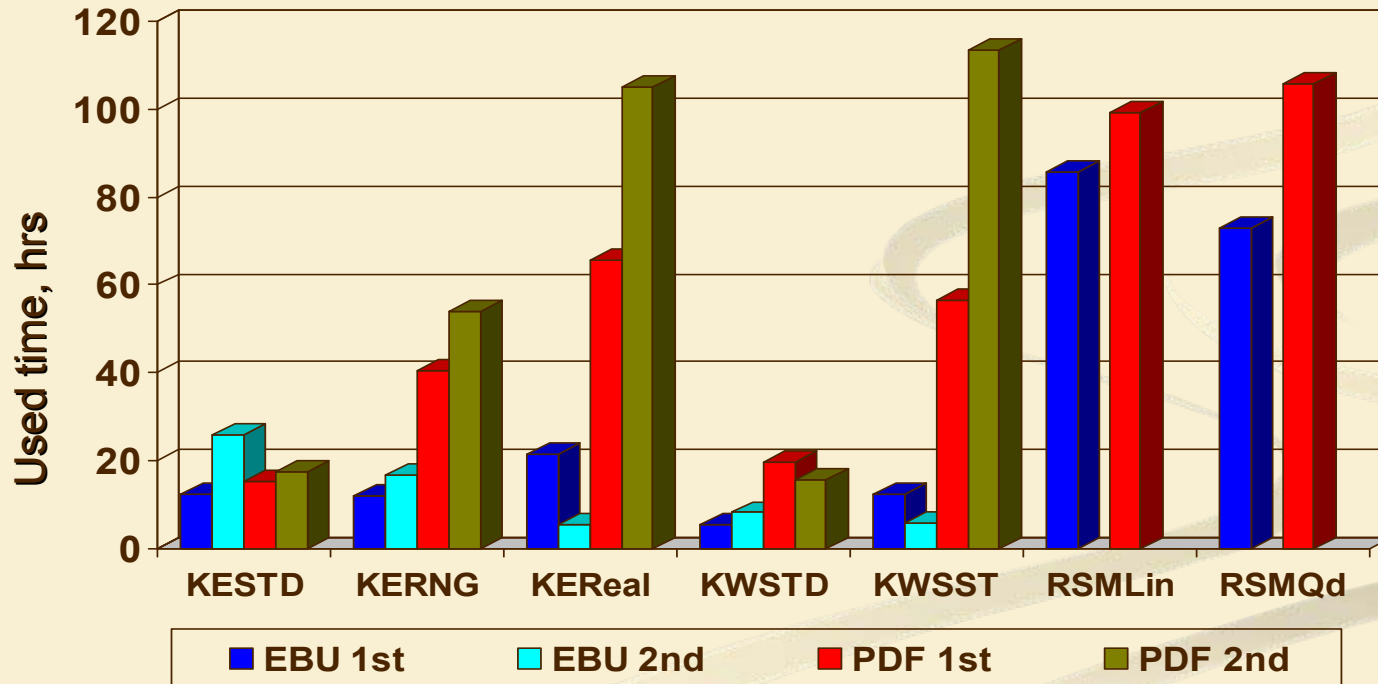
- ϵ cluster

Cores count:	16 (4 nodes)
Processors:	AMD Opteron 265
Memory:	8 Gb
Network connection:	Gigabit Ethernet
Peak performance:	35 GFLOPS
Operating system:	Windows CCS



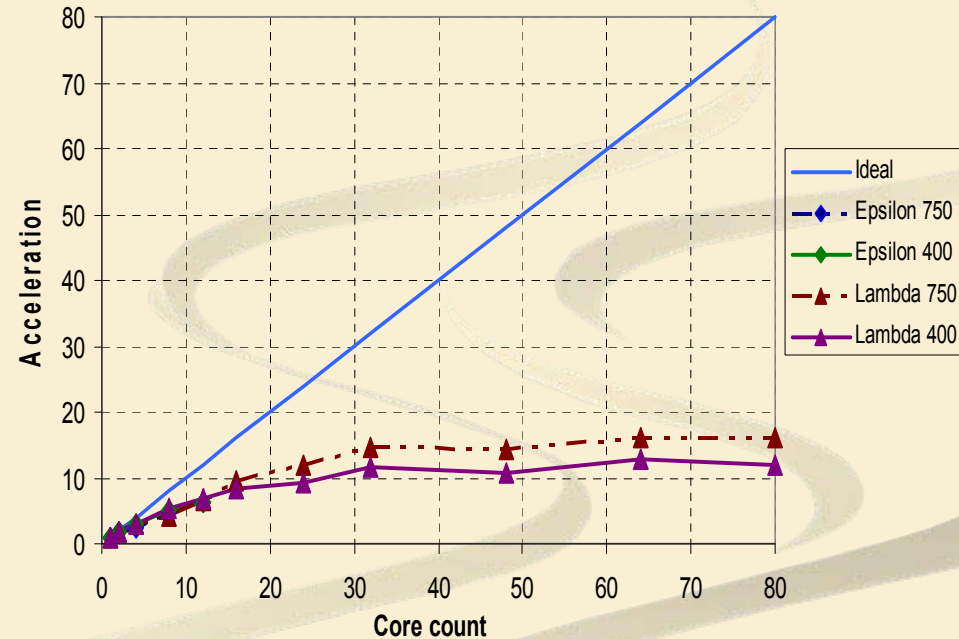
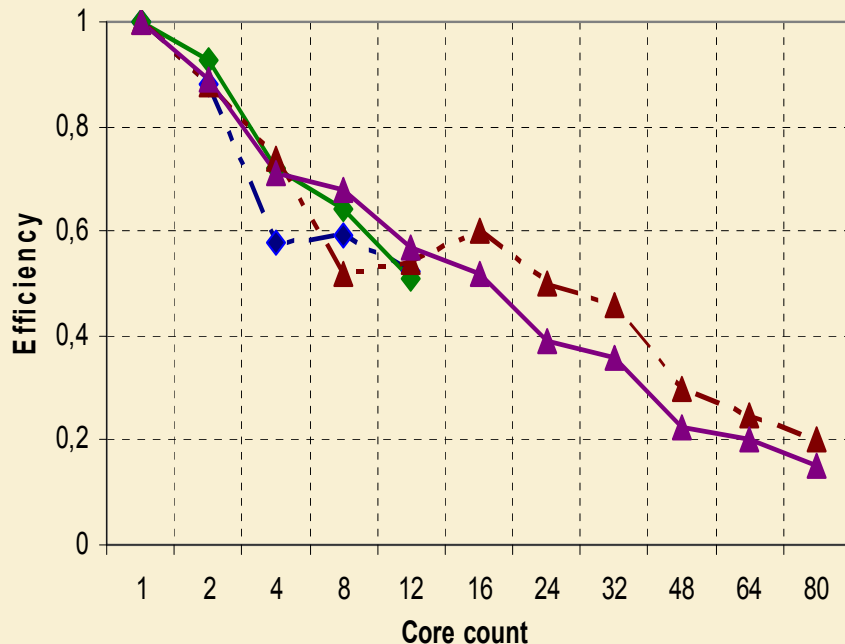
Models computational efficiency

- **Chemistry:** Eddy Break-up model is significantly faster than statistical model (PDF)
- **Turbulence:** RSM Quadratic Model is optimal stationary model
- **In general:** More accurate model requires more calculation time



Cluster computational efficiency

- *Windows CCS* and *Linux SUSE* have equal paralleling efficiency in this type of simulations
- ϵ cluster capabilities are insufficient for Large Eddy Simulations LES
- Computational time on λ -cluster: 5 weeks on 48 cores



Code efficiency

Fluent simulation

- 725 000 computational cells
- 16 (real) processors
- 25 000 time steps
- **840 hours**

Shekli et al.* simulation

- 930 000 computational cells
- 6 processors
- 50 000 time steps
- **110 hours**

$$\tilde{k} = \left(\frac{930000}{725000} \right)^3 \frac{1/6}{1/16} \frac{50000}{25000} \frac{1/110}{1/840} \approx 86$$

General conclusion:

Fluent specific code efficiency is 50 – 200 times poorer than in-house code

* - M.R.H. Sheikhi, T.G. Drozda, P. Givi, F.A. Jaber, S.B. Pope

“Large eddy simulation of a turbulent non-premixed piloted methane jet flame (Sandia Flame D)”, Proc. of Comb. Inst., 30, 2005

Conclusions

- Simple turbulence and chemistry models usage leads to severe errors in turbulent flame simulations
- Statistical Chemistry model significantly excels Eddy Break-up model
- RSM Quadratic, k - ϵ Realizable and k - ω SST stationary turbulence models are recommended
- Large Eddy Simulation provides lots of additional information but requires much computational time
- *Windows CCS* and *Linux SUSE* equals in paralleling efficiency on *Fluent* software

Future work

- Detailed research of flamelet chemistry models and reaction mechanisms
- Inspecting boundary perturbations impact on flame structure in *LES*
- Processors load balancing research
- Accurate pollutant emission models incorporation

Danke schön für Ihre Aufmerksamkeit!

